

Design and development of an interferometric readout for planetary seismometers

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Outline

- Introduction
- Context
- General principle
- PDH technique
- Work in progress
- Conclusion

Introduction

- Interior Exploration Using Seismic Investigation, Geodesy, and Heat Transport :
 - 2 instruments (1 designed by IPGP: SEIS (3 VBBs))
 - Composition & Structure of Earth-like planets + Formation & **Evolution**
 - Delayed mission (2018)
- Analytical model for mechanical transfer function of the SEIS • levelling system



VBB

=> Comparison between 2 different sensors: InSight's VBBs & optical seismometer

Context

- New generation of seismometers with improved performances :
 - Linearity
 - Noise level
- Expertise in APC : interferometric measurements at low frequencies and very low noise levels



⇒Objective : improve the sensibility by 2 orders of magnitude

Ex : InSight VBBs -> 4pm at 1 Hz







• EOM : phase modulation $\beta . \sin(\omega_m . t)$ Signal (1st order): $V(t) = V_0 . e^{i\omega t} + V_0 . \frac{\beta}{2} . e^{i(\omega + \omega_m)t} + V_0 . \frac{\beta}{2} . e^{i(\omega - \omega_m)t}$

• EOM : phase modulation $\beta.\sin(\omega_m.t)$

Signal (1st order): $V(t) = V_0 \cdot e^{i\omega t} + V_0 \cdot \frac{\beta}{2} \cdot e^{i(\omega + \omega_m)t} + V_0 \cdot \frac{\beta}{2} \cdot e^{i(\omega - \omega_m)t}$

Carrier

Sidebands

• EOM : phase modulation $\beta.\sin(\omega_m.t)$

Signal (1st order): $V(t) = V_0 \cdot e^{i\omega t} + V_0 \cdot \frac{\beta}{2} \cdot e^{i(\omega + \omega_m)t} + V_0 \cdot \frac{\beta}{2} \cdot e^{i(\omega - \omega_m)t}$

Carrier Sidebands Our case : 2 EOM => 8 sidebands



- E_r = reflected light out of the FP cavity
- E_{in} = incident light on the cavity Transfer Function

$$R(\omega) = \frac{E_r}{E_{in}} = \frac{-r_1 + (r_1^2 + t_1^2)r_2e^{i2\alpha}}{1 - r_1r_2e^{i2\alpha}}$$

With :

- \circ r : reflection coefficients of mirrors 1 and 2
- t1 : transmission coefficient of the mirror 1

$$\circ \alpha = \omega L/c$$



- E_{in} = incident light on the cavity
- Transfer Function

$$R(\omega) = \frac{E_r}{E_{in}} = \frac{-r_1 + (r_1^2 + t_1^2)r_2e^{i2\alpha}}{1 - r_1r_2e^{i2\alpha}}$$

New signal : unaltered sidebands + phase shifted carrier



• Power :

 $P_r = P_0 |R(\omega)|^2 + P_0 \frac{\beta^2}{4} \{ |R(\omega + \omega_m)|^2 + |R(\omega + \omega_m)|^2 \} + P_0 \beta \{ \operatorname{Re}[\chi(\omega)] \cos \omega_m t + \operatorname{Im}[\chi(\omega)] \sin \omega_m t \} + (2\omega_m terms) \}$

χ is a function of (ω - ω _{res})

• Extraction :





Work in progress

Mechanical prototype for cavity

| MAJOR CONSTRAINTS | |
|---|---|
| CONSTRAINT | SOLUTION |
| Vacuum resistance | Outgasing the material (under vacuum during a long period) before use |
| Minimization of cavity possible deformations under heat stress | Use of Invar material: good thermal properties, not expensive and possibility of complex shapes |
| Minimization of cavity possible deformations under vibratory stress (isolation in the range 10-2-1Hz) | Hopeless : no isolating materials at these frequencies! For the moment: isolation guaranteed above 10Hz + cylinder design (to maximise dynamical properties) and massive cavity (to increase eigenfrequency) |

Work in progress



Work in progress

- Next :
 - First resonating cavity
 - First noise measurements

Conclusion

- Noise level have to meet our expectations
- Performances comparison between InSight's VBBs & optical readout
- Final objective : optical seismometer prototype ≈ Next generation of planetary seismometers
- On Moon or Mars : better knowledge of internal structure

